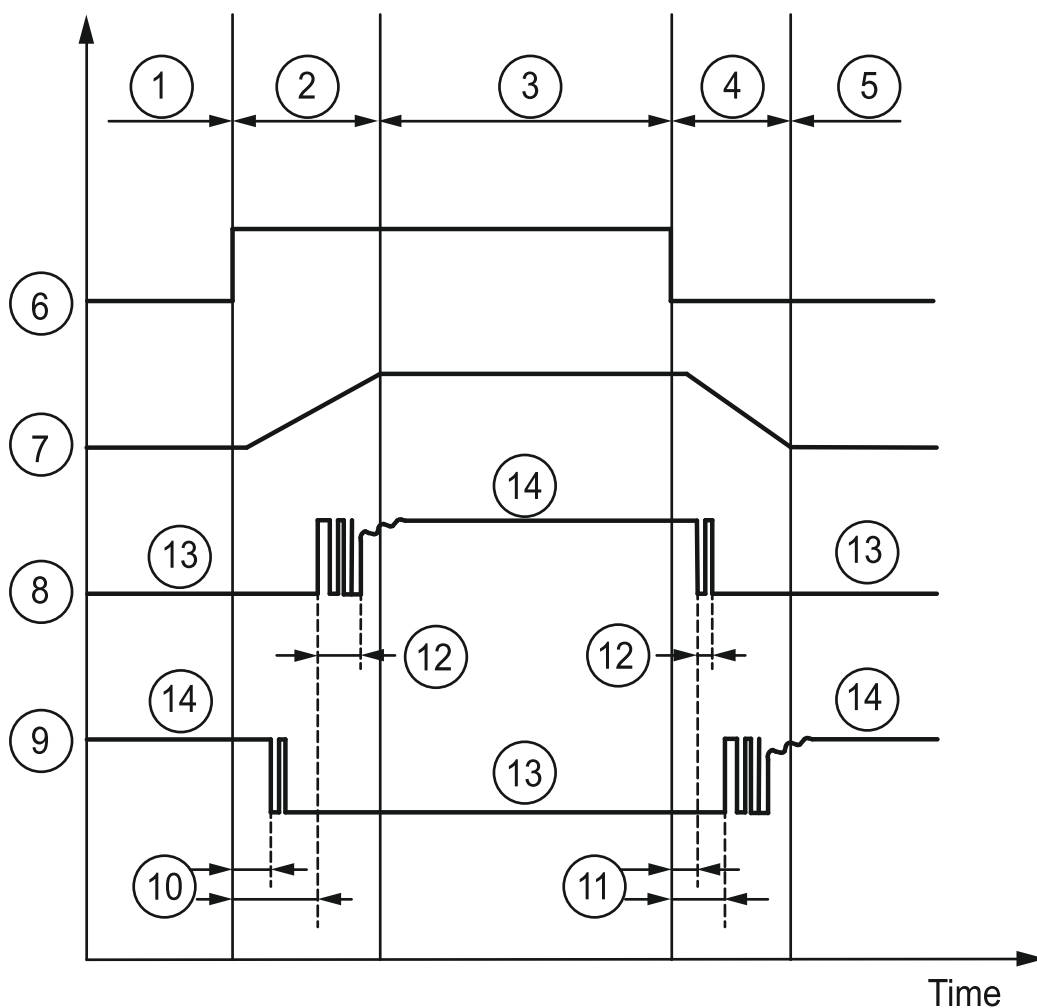


## Annex A (normative)

### Explanations regarding relays



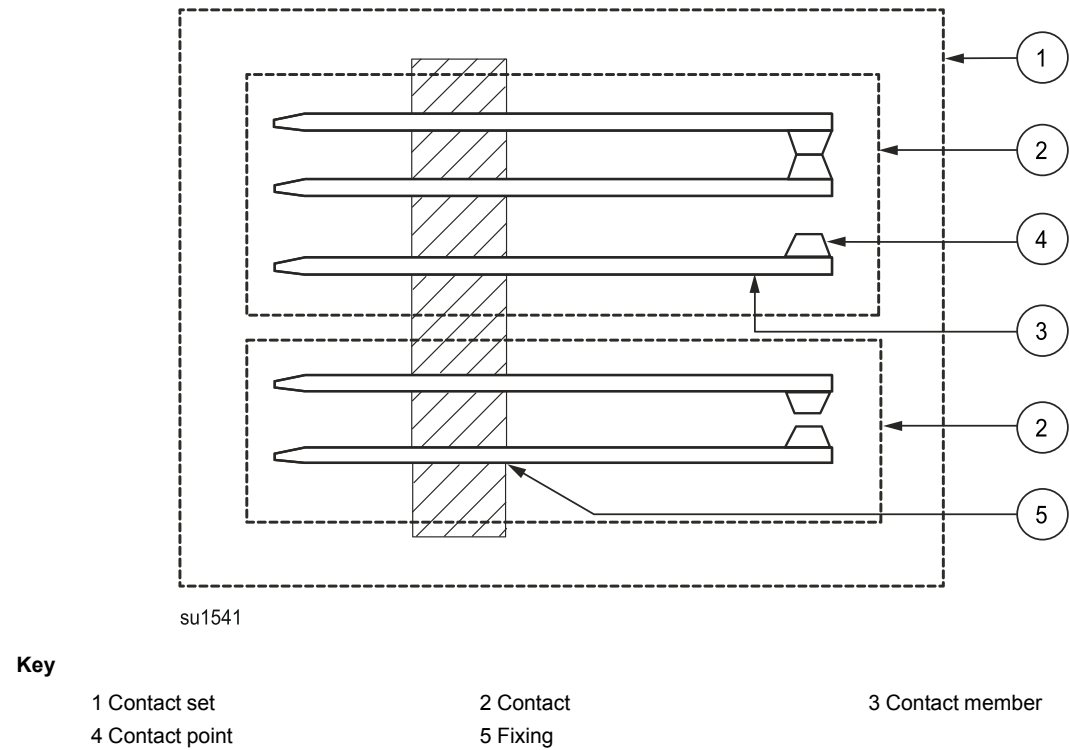
su1537

#### Key

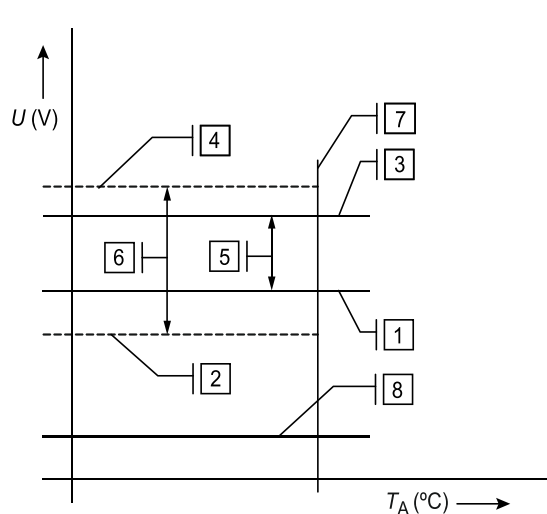
1 Release condition	8 Voltage at make contact
2 Operate	9 Voltage at break contact
3 Operate condition	10 Operate time
4 Release	11 Release time
5 Release condition	12 Bounce time
6 Coil voltage	13 Open
7 Change in position of movable parts	14 Closed

**Figure A.1**

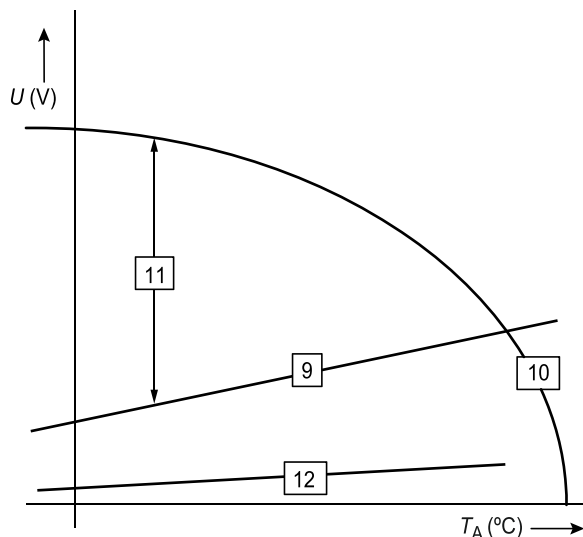
**Diagram explaining terms related to monostable relays**



**Figure A.2**  
**Example explaining terms relating to contacts**



su1542

Operative range according to [5.3.1](#)Operative range according to [5.3.2](#)**Key** $U$  Coil voltage $T_A$  Ambient temperature

1 Rated coil voltage, or lower limit of the rated coil voltage range

2 Lower limit of the operative range of the coil voltage  
EXAMPLE 80 % of 1 (for class 1)

3 Rated coil voltage, or upper limit of the rated coil voltage range

4 Upper limit of the operative range of the coil voltage  
EXAMPLE 110 % of 3 (for class 1)

5 Rated coil voltage range

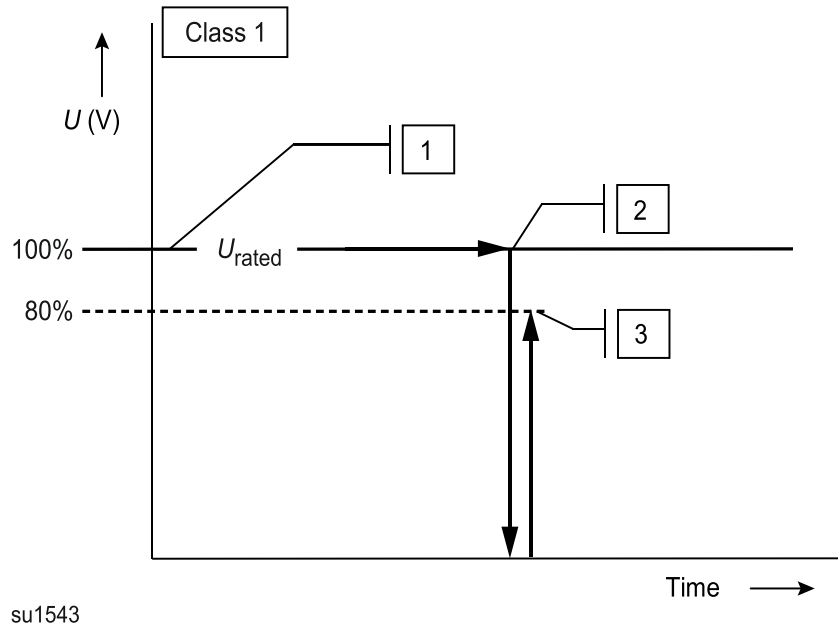
6 Operative range of the coil voltage

7 Maximum permissible ambient temperature for the rated coil voltage or the rated coil voltage range

8 Release voltage,  $\geq 5\%$  (DC coil) /  $15\%$  (AC coil) of 39 Lower limit  $U_1$  of the operative range of the coil voltage10 Upper limit  $U_2$  of the operative range of the coil voltage (limiting voltage)

11 Operative range of the coil voltage

12 Release voltage,  $\geq 10\%$  (DC coil) /  $15\%$  (AC coil) of 9**Figure A.3****Explanations regarding the operative range of the coil voltage**

**Key**

1 Energization with rated coil voltage (or upper limit of rated coil voltage range) until thermal equilibrium is reached

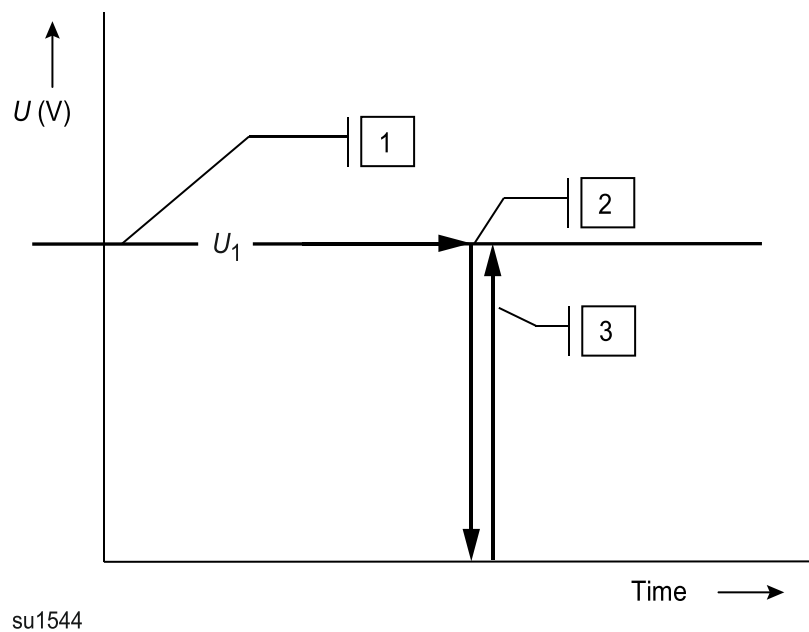
2 Removal of voltage

3 Immediately after the removal of the coil voltage, energization with 80 % of the rated coil voltage (or lower limit of rated coil voltage range)

Requirement: the relay shall operate

**Figure A.4**

**Explanation regarding the preconditioning and testing of the operate voltage according to [5.3.1](#) (Class 1) and [9.2](#)**

**Key**

1 Energization with the maximum value of the lower limit  $U_1$  of the operative range of the coil voltage until thermal equilibrium is reached

2 Removal of voltage

3 Immediately after the removal of the coil voltage, re-energization with  $U_1$

Requirement: the relay shall operate

**Figure A.5**

**Explanation regarding the preconditioning and testing of the operate voltage according to [5.3.2](#) and [9.2](#)**

## Annex B (informative)

### Inductive contact loads

#### **Annex BDV D2 Modification to Annex [B](#):**

**Annex [B](#) is normative.**

In this annex provisions for the testing of relays with respect to making and breaking capacity and electrical endurance for inductive contact loads are specified. Other loads and tests may be specified by the manufacturer.

Unless otherwise specified the testing is carried out at ambient temperature.

Separate samples may be used for the different tests of [Table B.1](#) to [Table B.3](#).

The sample lot shall be chosen in accordance with [Table 5](#), test procedure B for [Table B.1](#) and [Table B.2](#) and for [Table B.3](#) test procedure A only.

It is up to the discretion of the manufacturer to choose one or more of the tests described in [Table B.1](#), [Table B.2](#) and [Table B.3](#), respectively. However, when the test according to [Table B.1](#) is performed, also the test of [Table B.2](#) applies.

The performed test(s) are to be indicated in the test report.

NOTE In the following tables a classification of loads is given, related to utilization categories (AC 15 and DC 13) defined in IEC 60947-5-1.

For the electrical endurance test the duty factor shall be not more than 50% but not less than 10% and the 10 times making current shall not overheat the test device.

The test circuit shall be in accordance with [C.1](#). In addition a resistor shall be in parallel to the breaking load carrying 3% (for AC and 1% for DC) of the breaking current. The inductance shall be provided by air core reactors or alternatively with iron core reactors (with a maximum distortion factor of 5% for AC). If the contact bouncing is less than 3 ms it is permitted to carry out the electrical endurance only with the breaking load (without the higher inrush load).

NOTE: Provisions for measuring the contact bounce time can be found in IEC 61810-7.

#### **BDV.1 D2 Modify Annex [B](#) by adding the following:**

**BDV.1 Test procedure B requires verification of the making and breaking capacity under normal conditions ([Table B.2](#)). As a result of this test, there shall be no:**

- a) Electrical or mechanical breakdown of the device;
- b) Undue burning or pitting of the contacts; or
- c) Welding of the contacts

**BDV.2 The representative load for the overload and making and breaking capacity tests shall be one of the following types:**

- a) An electromagnetic load in accordance with the applicable load type values per [Table B.2](#); or

b) An electromagnetic load based on the manufacturer's declared values for operational current,  $I_e$  and operational voltage,  $U_e$ . Unless otherwise known, the ac making current is to be ten times the steady state current.

**BDV.3** In lieu of the electromagnetic loads described in [BDV.2](#), an air-core inductive load may be used to produce the making and breaking currents in [Table B.2](#), provided the duration of the making current shall be at least two cycles at 50 or 60 hertz.

**BDV.4** An air-core inductive load may be connected in parallel with a resistor if the resistor ( $R_{SH}$ ) power consumption is approximately 3 percent of the total power consumption calculated in accordance with the following formula:

$$R_{SH} = 33.3 (1 / PF - PF) \cdot E / I$$

In which:

PF is the power factor;

E is the closed-circuit phase voltage; and

I is the phase current.

**Table B.1**  
Verification of the making and breaking capacity (abnormal conditions)

Classification	Making			Breaking			Number of cycles and frequency		
	$I/I_e$	$U/U_e$	$\cos \varphi$	$I/I_e$	$U/U_e$	$\cos \varphi$	Number of cycles	Frequency in cycles per minute	Duration of energization s
AC inductive load (contactor coil, solenoid valve)	10	1,1	0,3	10	1,1	0,3	10	6	0,04
	Total number of cycles						10		
	$I/I_e$	$U/U_e$	$T_{0,95}$	$I/I_e$	$U/U_e$	$T_{0,95}$	Number of cycles	Frequency in cycles per minute	Duration of energization
DC inductive load (contactor coil, solenoid valve)	1,1	1,1	$6 \times P^a$	1,1	1,1	$6 \times P^a$	10	6	$T_{0,95}$
	Total number of cycles						10		
$I_e$	Rated operating current					$I$	Switching current		
$U_e$	Rated operating voltage					$U$	Switching voltage		
$P = U_e \times I_e$	Steady-state power in W					$T_{0,95}$	Time to reach 95 % of the steady-state current in ms		
<sup>a</sup> The value "6 × P" is derived from an empirical relation appropriate for most of the d.c. inductive loads up to P = 50 W, where 6 × P = 300 ms. Loads with a rated power above 50 W comprise small loads in parallel. Therefore, 300 ms is an upper limit independent of the power value.									

**Table B.2**  
**Verification of the making and breaking capacity (normal conditions)**

Classification	Making			Breaking			Number of cycles and frequency		
	$I/I_e$	$U/U_e$	$\cos \varphi$	$I/I_e$	$U/U_e$	$\cos \varphi$	Number of cycles	Frequency in cycles per minute	Duration of energization s
AC inductive load (contactor coil, solenoid valve)	10	c	0,3	1	c	0,3	50	6	0,05
	10	1	0,3	1	1	0,3	10	> 60 <sup>b</sup>	0,05
	10	1	0,3	1	1	0,3	990	60	0,05
	10	1	0,3	1	1	0,3	5 000	6	0,05
	Total number of cycles						6 050		
	$I/I_e$	$U/U_e$	$T_{0,95}$	$I/I_e$	$U/U_e$	$T_{0,95}$	Number of cycles	Frequency in cycles per minute	Duration of energization
DC inductive load (contactor coil, solenoid valve)	1	c	$6 \times P^a$	1	c	$6 \times P^a$	50	6	$T_{0,95}$
	1	1	$6 \times P^a$	1	1	$6 \times P^a$	10	> 60 <sup>b</sup>	$T_{0,95}$
	1	1	$6 \times P^a$	1	1	$6 \times P^a$	990	60	$T_{0,95}$
	1	1	$6 \times P^a$	1	1	$6 \times P^a$	5 000	6	$T_{0,95}$
	Total number of cycles						6 050		
$I_e$	Rated operating current			$I$	Switching current				
$U_e$	Rated operating voltage			$U$	Switching voltage				
$P = U_e \times I_e$	Steady-state power in W			$T_{0,95}$	Time to reach 95 % of the steady-state current in ms				

<sup>a</sup> The value " $6 \times P$ " is derived from an empirical relation appropriate for most of the d.c. inductive loads up to  $P = 50$  W, where  $6 \times P = 300$  ms. Loads with a rated power above 50 W comprise small loads in parallel. Therefore, 300 ms is an upper limit independent of the power value.

<sup>b</sup> With maximum permissible frequency (ensuring reliable making and breaking of the contacts).

<sup>c</sup> The test is carried out at a voltage of  $U_e \times 1,1$ , with the test current  $I_e$  adjusted at  $U_e$ .

**Table B.3**  
**Electrical endurance test**

Current	Classification	Making			Breaking		
AC	inductive load (contactor coil, solenoid valve)	$I$	$U$	$\cos \varphi$	$I$	$U$	$\cos \varphi$
		$10 I_e$	$U_e$	0,7 <sup>a</sup>	$I_e$	$U_e$	0,4 <sup>a</sup>
DC <sup>b</sup>	inductive load (contactor coil, solenoid valve)	$I$	$U$	$T_{0,95}$	$I$	$U$	$T_{0,95}$
		$I_e$	$U_e$	$6 \times P^c$	$I_e$	$U_e$	$6 \times P^c$
$I_e$	Rated operating current			$I$	Switching current		
$U_e$	Rated operating voltage			$U$	Switching voltage		
$P = U_e \times I_e$	Steady-state power in W			$T_{0,95}$	Time to reach 95 % of the steady-state current in ms		

<sup>a</sup> The power factors indicated are conventional values and appear only in test circuits in which electrical characteristics of coils are simulated. Reference is made to the fact that for circuits with a power factor of 0,4 shunt resistors are used to simulate the damping effect due to eddy current losses.

<sup>b</sup> For d.c. inductive loads provided with a switching device to operate an economy resistor, the rated operating current shall be equal to at least the highest making current.

<sup>c</sup> The value " $6 \times P$ " is derived from an empirical relation appropriate for most of the d.c. inductive loads up to  $P = 50$  W, where  $6 \times P = 300$  ms. Loads with a rated power above 50 W comprise small loads in parallel. Therefore, 300 ms is an upper limit independent of the power value.



**Table B.4**  
**Contact rating designations and equivalency to utilization categories**

Designation <sup>a</sup>	Utilization category	Conventional enclosed thermal current $I_{the}$ A	Rated operational current $I_e$ (A) at rated operational voltage $U_e$						VA rating <sup>b</sup>		
<i>Alternate current</i>		10 10 10 5 5 5 2,5 2,5 2,5 1,0 1,0 0,5	120 V	240 V	380 V	480 V	500 V	600 V	M	B	
A150	AC – 15		6	–	–	–	–	–	7 200	720	
A300	AC – 15		6	3	–	–	–	–	7 200	720	
A600	AC – 15		6	3	1,9	1,5	1,4	1,2	7 200	720	
B150	AC – 15		3	–	–	–	–	–	3 600	360	
B300	AC – 15		3	1,5	–	–	–	–	3 600	360	
B600	AC – 15		3	1,5	0,95	0,75	0,72	0,6	3 600	360	
C150	AC – 15		1,5	–	–	–	–	–	1 800	180	
C300	AC – 15		1,5	0,75	–	–	–	–	1 800	180	
C600	AC – 15		1,5	0,75	0,47	0,375	0,35	0,3	1 800	180	
D150	AC – 14		0,6	–	–	–	–	–	432	72	
D300	AC – 14		0,6	0,3	–	–	–	–	432	72	
E150	AC – 14		0,3	–	–	–	–	–	216	36	
<i>Direct current</i>			10 10 10 5 5 5 2,5 2,5 2,5 1,0 1,0	125 V	250 V		400 V	500 V	600 V		
N150	DC-13			2,2	–		–	–	–	275	275
N300	DC-13	2,2		1,1		–	–	–	275	275	
N600	DC-13	2,2		1,1		0,63	0,55	0,4	275	275	
P150	DC-13	1,1		–		–	–	–	138	138	
P300	DC-13	1,1		0,55		–	–	–	138	138	
P600	DC-13	1,1		0,55		0,31	0,27	0,2	138	138	
Q150	DC-13	0,55		–		–	–	–	69	69	
Q300	DC-13	0,55		0,27		–	–	–	69	69	
Q600	DC-13	0,55		0,27		0,15	0,13	0,1	69	69	
R150	DC-13	0,22		–		–	–	–	28	28	
R300	DC-13	0,22	0,1		–	–	–	28	28		
									M = make B = break		
a The letter stands for the conventional enclosed thermal current and identifies (a.c. or d.c.): for example B means 5 A a.c. The rated insulation voltage $U_i$ is at least equal to the number after the letter.											
b The rated operational current $I_e$ (A), the rated operational voltage $U_e$ (V) and the break apparent power B (V.A) are correlated by the formula $B = U_e \times I_e$ .											

## Annex C (normative)

### Test set-up

#### Annex CDV D2 Modification to Annex C:

Annex C is normative.

### C.1 Test circuit

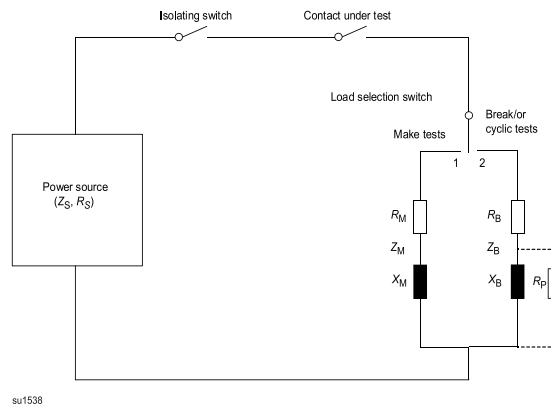
A generalized test circuit is given in [Figure C.1](#) and a functional block diagram in [Figure C.2](#).

NOTE The isolating switch, the load selection switch and the contact under test shall be sequenced appropriate to the test conditions specified.

The characteristics indicated in [Table C.1](#) and [Table C.2](#) apply, unless otherwise specified.

The test conditions given in Clause apply. All relevant details (e. g. number of cycles, frequency of operation, duration of energization) have to be specified by the manufacturer.

The declared value of the current shall be expressed in terms of the steady state (r.m.s. if a.c.) value of current in the contact circuit.



Contact categories 0 and 1

$$Z_s < 0,02 Z_{M,B} \text{ (a.c.)}$$

$$R_s < 0,02 R_{M,B} \text{ (d.c.)}$$

Contact category 2

$$Z_s < 0,05 Z_{M,B} \text{ (a.c.)}$$

$$R_s < 0,05 R_{M,B} \text{ (d.c.)}$$

For standard load values and tolerances for  $L/R$  and  $\cos \varphi$ : see [Table C.2](#).

Load selection switch, position 1: Make test when different load (inrush current) is used.

Load selection switch, position 2: Make and break (or cyclic) tests with same load.

Isolating switch: Used to connect/disconnect the load circuit, independent of the contact under test.

Formula for  $R_P$ :  $R_P = 33,3 \times (1 / \cos \varphi - \cos \varphi) \times U / I_e$

**Figure C.1**  
**Standard test circuit**